## Energy dissipation and hysteresis cycles in pre-sliding transients of kinetic friction

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May 24, 2022

The problem of transient hysteresis cycles due to pre-sliding friction is of importance for the analysis and identification of micro- and nano-positioning instruments and devices and their precisely controlled operation. The convergence to zero equilibrium under nonlinear frictional damping appears to bear nontrivial trajectory solutions, cf. [7], that can degrade the control performance by inducing multiple pre-sliding cycles before attaining final zero velocity. Obviously, even an unforced motion dynamics

$$m\frac{d^2x}{dt^2} + h\left[\frac{dx}{dt}, t\right] = 0, \quad \frac{dx}{dt}(0) \neq 0 \tag{1}$$

of the point mass m, which is damped by the nonlinear friction  $h(\cdot)$  with hysteresis, requires a series of piecewise continuous solutions on the intervals  $[t_i, \ldots, t_{i+1}]$ , where i is the index of consecutive reversals of a relative displacement. The formal proof of stability and, therefore, type of convergence of  $dx/dt \rightarrow 0$  in (1) is nontrivial and depends on the analytic form of frictional hysteresis map  $h(\cdot)$  and its parametrization, also with respect to m. To find a suitable Lyapunov function candidate for (1) is not always possible for an assumed  $h(\cdot)$ . For the distributed Maxwell-slip friction model, which is equivalent to the Prandtl-Ishlinskii (PI) stop-type hysteresis operator and allows for describing the Coulomb friction with pre-sliding cf. [6], such Lyapunov-based analysis was demonstrated in [1]. However, for a finite elements realization, at least one PI element should have infinite stiffness, thus approaching sign(dx/dt)for guaranteing convergence and avoiding stable limit cycles of (1). For more compact, in terms of dimension of the parameters space, and piecewise smooth friction models, like the well-celebrated Dahl one [3] and the hysteresis-area oriented tribological one [4], an easy-to-handle candidate for the Lyapunov function may not exist, or at least cannot be found with the given analysis tools. Motivated by the way of analysis [5] of mechanical systems with frictional hysteresis, we will consider the (x, h) phase-plane for which (1) can be transformed to

$$m \int_{\dot{x}_{i}}^{\dot{x}_{i+1}} \dot{x} d\dot{x} = -\int_{x_{i}}^{x_{i+1}} h(\dot{x}, t) dx = 0.$$
(2)

Assuming, without loss of generality, the pre-sliding initial condition  $x_i(0) = 0$ and taking into account that  $\dot{x}_i = \dot{x}_{i+1} = 0$  for each pair of the consecutive

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motion reversals, the evaluation of both integrals in (2) allows analyzing the pre-sliding hysteresis cycles. At each period of the pre-sliding cycles, the kinetic energy  $E_k = 0.5 m \dot{x}^2$  is balanced by the energy of hysteresis  $E_h = \int_{x_i}^x h(\cdot) dx$ , while the latter consists of the recuperative potential part  $E_p$  and dissipative damping part  $E_d$ , so that  $E_h = E_p + E_d$ . From the energy conservation viewpoint, it is obvious that the kinetic energy will grow, and thus  $|\dot{x}(t)|$  increases as long as  $\operatorname{sign}(\dot{x}) = -\operatorname{sign}(h)$ , while  $|\dot{x}(t)|$  starts to decrease as long as the sign of velocity and friction force becomes the same. Respectively, it applies  $\max |\dot{x}| = |\dot{x}(t_0)|$ , where  $t_i < t_0 < t_{i+1}$  is the time instant of  $h(\cdot) = 0$ . The above developments allow calculating both, the energy dissipation during presliding cycles driven by the hysteresis, and the size and period of these cycles. We will analyze two piecewise smooth pre-sliding hysteresis mappings, one of the Dahl model [3] and another one of the hysteresis-area based model, as it is provided in [2]. Both can be seen as a tribology- and engineering-motivated extension of the classical Coulomb friction law, that captures the pre-sliding hysteresis transitions and, this way, avoids discontinuity in  $h(\cdot)$  at the velocity zero crossing. Outside the pre-sliding range and until the next  $t_i$ , both models saturate at the Coulomb friction level  $F_c$  and reduces the system dynamics (1) to the  $m\ddot{x} = -F_c \operatorname{sign}(\dot{x})$  form.

## References

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